



*Current status of
the CAM dynamical cores
and ~~vertical resolution~~*

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Atmospheric Modeling and Prediction (AMP) Section
Climate and Global Dynamics (CGD) Laboratory
National Center for Atmospheric Research (NCAR)

**CESM Atmosphere / Whole Atmosphere / Chemistry-Climate
WINTER WORKING GROUP MEETING, February 7-10**



Current status of the CAM dynamical cores and enthalpy flux plans

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Getting away from CAM-FV ...



CAM-FV (finite volume)

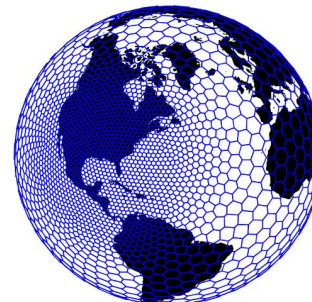
Lin (2004)

CAM-EUL/SLD



CAM-SE (spectral elements)

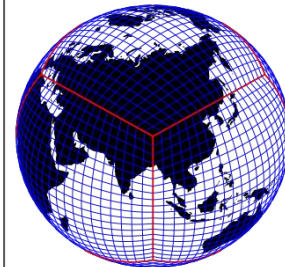
Taylor et al., (1997)
Dennis et al., (2012)



CAM-MPAS (Model for Prediction Across Scales)

Skamarock et al., (2012)

Available in CAM since 2020:



CAM-FV3
(GFDL/NOAA global dynamical core)

Available in CAM since 2021

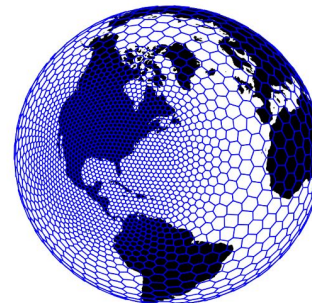
No active development in over a decade



Getting away from CAM-FV ...



CAM-SE (spectral elements)
Taylor et al., (1997)
Dennis et al., (2012)

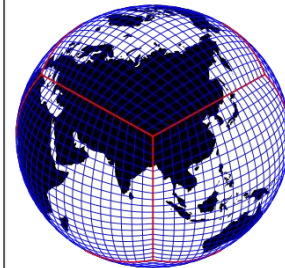


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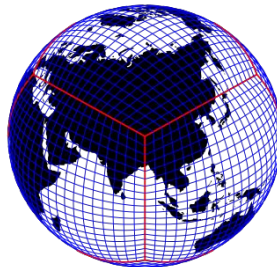
No active development in over a decade

- used for vertical advection in single-column setup (inconsistent from numerical methods/consistency point of view - should be consistent with dycore being used in 3D model)
- popular dynamical core for dynamicists (and ultra fast on small machines/clusters)

FV ...



CAM-SE (spectral elements)
Taylor et al., (1997)
Dennis et al., (2012)

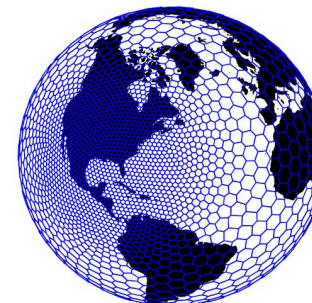


CAM-FV3
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CAM-FV (finite volume)
Lin (2004)

~~CAM-EUL/SLD~~



CAM-MPAS (Model for Prediction Across Scales)
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Available in CAM since 2021

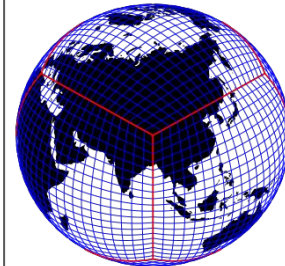
No active development in over a decade



Getting a...

- Dycore was used for IPCC (CESM2) so likely will be needed as a reference for a while!
- Used for low resolution (e.g. paleo, low res WACCM) applications
(could SE do that? Need "extreme" scalability at low res for fast throughput!)

Available in CAM since 2020:



CAM-FV3
(GFDL/NOAA global dynamical core)

Available in CAM since 2021

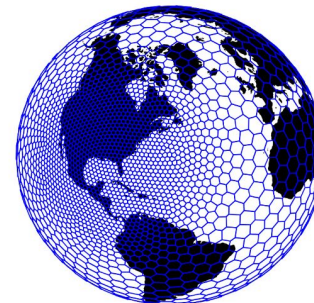


CAM-FV (finite volume)
Lin (2004)

CAM-EUL/SLD



CAM-SE (spectral elements)
Taylor et al., (1997)
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CAM-MPAS (Model for Prediction Across Scales)
Skamarock et al., (2012)

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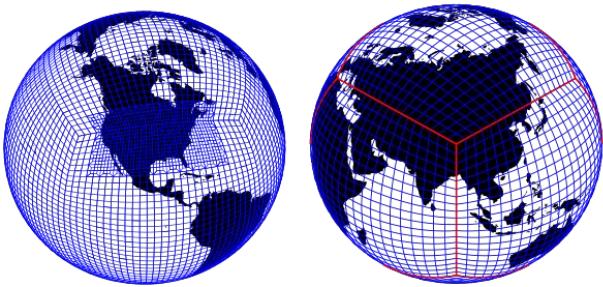
Next generation dycore implementation for climate

Current status with respect to CAM7 (new vertical resolution)

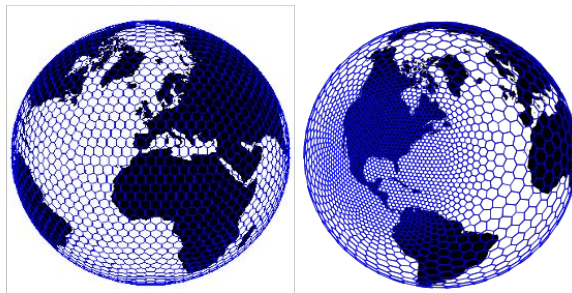


- **SE: Fully functional with new vertical resolution**
(FYI: NOAA seed project for developing SE for Mars funded - *CESM Alternative Earths effort*)
- **MPAS: Fixed some physics-dynamics coupling issues (at high horizontal resolution); implementing frontogenesis functions (needed for ~80km and higher top); setup new vertical resolution** (FYI: lots going on for high resolution and high top - see SIMA and EarthWorks presentations later today)
- **FV3: Upgrading to new GFDL code base; implementing frontogenesis functions; setup new vertical resolution**

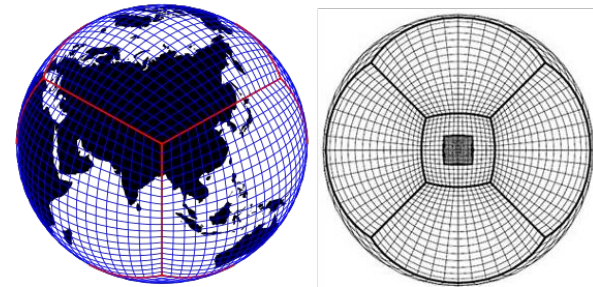
CAM-SE(CSLAM)



CAM-MPAS



CAM-FV3





“Enthalpy flux” plans



- Why? The upper boundary condition for MOM6 ocean model requires explicit specification of the heat fluxes associated with water leaving/entering the ocean (a.k.a. enthalpy fluxes)
- Why? Enthalpy fluxes neglected in CAM energy budgets; effectively in CAM’s global energy fixer
- see AMWG talk 2021: <https://www.cgd.ucar.edu/cms/pel/papers/L2021AMWG.pdf> or Lauritzen et al. (2022, in prep)

Note: If one naively adds flux terms to CAM and does nothing else, one can easily introduce energetic and thermodynamic inconsistencies in the coupled system so we have to be very careful on how we proceed ...



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Note: If one naively adds flux terms to CAM and does nothing else, one can easily introduce energetic and thermodynamic inconsistencies in the coupled system so we have to be very careful on how we proceed ...



JAMES | Journal of Advances in Modeling Earth Systems

Reconciling and improving formulations for thermodynamics and conservation principles in Earth System Models (ESMs)

P.H. Lauritzen¹, N.K.-R. Kevlahan², C. Eldred³, T. Dubos⁴, A. Gassmann⁵, T. Toniazzo⁶, B.E. Harrop⁷, A.R. Herrington¹, V.E. Larson⁸, B. Shipway⁹, O. Guba³, F. Lemarié¹⁰, R. Tailleux¹¹, C. Jablonowski¹², W. Large¹, P.J. Rasch⁷, A.S. Donahue¹³, H. Wan⁷, A. Conley¹, H. Johansen¹³, K. Roy¹⁴

Note: Discusses CLUBB-CAM thermodynamic consistency that A. Herrington mentioned in his talk!



Total energy equation



Lauritzen et al. (2022, in prep)

Assume:

- Primitive equations (hydrostatic, shallow atmosphere, ideal gas)
- Assume model top pressure is constant
- All components of moist air have the **same temperature** and move with the **same horizontal velocity**
- Assume that water entering the atmosphere (evaporation, snow drift, sea spray) has **same temperature** as water leaving the atmosphere (dew, liquid and frozen precipitation) **DEFINITELY NOT ALWAYS ACCURATE!**

Then it can be shown that the following globally integrated total energy equation holds:

$$\frac{\partial}{\partial t} \iiint \rho^{(d)} \left\{ K + \Phi_s + c_p^{(d)} T + \sum_{\ell \in \mathcal{L}_{H_2O}} m^{(\ell)} \left[K + \Phi_s + c_p^{(\ell)} (T - T_{00}) + h_{00}^{(ice)} \right] + m^{(wv)} L_{s,00} + m^{(liq)} L_{f,00} \right\} dA dz$$

$$= \iint \left\{ \sum_{\ell \in \mathcal{L}_{H_2O}} F_{net}^{(\ell)} \left[\tilde{K}_s + \Phi_s + c_p^{(\ell)} (\tilde{T}_s - T_{00}) + h_{00}^{(ice)} \right] + F_{net}^{(wv)} L_{s,00} + F_{net}^{(liq)} L_{f,00} + F_{net}^{(turb,rad)} \right\} dA. \quad (94)$$

symbol	description	unit
$c_p^{(\ell)}$	heat capacity at constant pressure of species ℓ	J/K/kg
$F_{net}^{(\ell)}$	net flux of water species ℓ into the atmosphere	kg/m ² /s
$F_{net}^{(turb,rad)}$	Radiative and sensible/turbulent fluxes into atmosphere (90)	J/m ² /s
$h_{00}^{(ice)}$	reference enthalpy for water form ℓ	J/kg
$m^{(\ell)}$	dry mixing ratio ($\equiv \rho^{(\ell)}/\rho^{(d)}$)	kg/kg
K	specific horizontal kinetic energy ($\equiv \frac{1}{2} \tilde{v}^2$)	m ² /s ²
$L_{f,00}$	latent heat of fusion	J/K
$L_{s,00}$	latent heat of sublimation	J/K
$L_{v,00}$	latent heat of vaporization	J/K
Φ_s	surface geopotential	m ² /s ²
ρ_d	dry air density	kg/m ³
T	temperature	K
\tilde{T}_s	common temperature at surface	K
\tilde{v}	horizontal velocity vector	m/s

(ice reference enthalpy, $\tilde{T}_s \equiv T_{atm,s} = T_{surf,s}$)

now also assume that the energy equation is valid for grid mean values in the model (**QUESTIONABLE ASSUMPTION!**)



Total energy equation

Assume:

- Primitive equations (hydrostatic, shallow atmosphere, ...)
- Assume model top pressure is constant
- All components of moist air have the **same temperature**
- Assume that water entering the atmosphere (evaporation) ... leaving the atmosphere (dew, liquid and frozen precipitation) ...

Total water held fixed during physics parameterizations; updated at end of physics and the energy associated with water changes stays in the atmosphere (in the form of a global uniform temperature increment)

Lauritzen et al. (2022, in prep)

al velocity
temperature as water
ACCURATE!

Then it can be shown that the following globally integrated to

Many models make these assumptions:

$$\frac{\partial}{\partial t} \iiint \rho^{(d)} \left\{ \bar{K} + \bar{\Phi}_s + c_p^{(d)} \bar{T} + \sum_{\ell \in \mathcal{L}_{H_2O}} m^{(\ell)} \left[\bar{K} + \bar{\Phi}_s + c_p^{(\ell)} (\bar{T} - T_{00}) + h_{00}^{(ice)} \right] + \bar{m}^{(wv)} L_{s,00} + \bar{m}^{(liq)} L_{f,00} \right\} dA dz$$

$$= \iint \left\{ \sum_{\ell \in \mathcal{L}_{H_2O}} \bar{F}_{net}^{(\ell)} \left[\bar{\tilde{K}}_s + \bar{\Phi}_s + c_p^{(\ell)} (\bar{\tilde{T}}_s - T_{00}) + h_{00}^{(ice)} \right] + \bar{F}_{net}^{(wv)} L_{s,00} + \bar{F}_{net}^{(liq)} L_{f,00} + \bar{F}_{net}^{(turb,rad)} \right\} dA.$$

(ice reference enthalpy, $\bar{\tilde{T}}_s \equiv \bar{T}_{atm,s} = \bar{T}_{surf,s}$)

(94) ←

Now also assume that the energy equation is valid for grid mean values in the model (QUESTIONABLE ASSUMPTION!)



“Enthalpy flux” plan

Assume:

- Primitive equations (hydrostatic, shallow atmosphere, ideal gas)
- Assume model top pressure is constant
- All components of moist air have the **same temperature** and move with the **same horizontal velocity**
- Precipitation falling through the atmosphere (evaporation, snow drift, sea spray) has **same temperature** as water
- Precipitation (rain, dew, liquid and frozen precipitation) **DEFINITELY NOT ALWAYS ACCURATE!**

Lauritzen et al. (2022, in prep)

incl. all forms of water in lhs. terms

(small energy budgets change - Lauritzen et. al (2022))

Many models make these assumptions:

$$\frac{\partial}{\partial t} \iiint \rho^{(d)} \left\{ \bar{K} + \bar{\Phi}_s + c_p^{(d)} \bar{T} + \sum_{\ell \in \mathcal{L}_{H_2O}} m^{(\ell)} \left[\bar{K} + \bar{\Phi}_s + c_p^{(\ell)} (\bar{T} - T_{00}) + h_{00}^{(ice)} \right] + \bar{m}^{(wv)} L_{s,00} + \bar{m}^{(liq)} L_{f,00} \right\} dA dz$$

$$= \iint \left\{ \sum_{\ell \in \mathcal{L}_{H_2O}} \bar{F}_{net}^{(\ell)} \left[\bar{\tilde{K}}_s + \bar{\Phi}_s + c_p^{(\ell)} (\bar{\tilde{T}}_s - T_{00}) + h_{00}^{(ice)} \right] + \bar{F}_{net}^{(wv)} L_{s,00} + \bar{F}_{net}^{(liq)} L_{f,00} + \bar{F}_{net}^{(turb,rad)} \right\} dA.$$

$\mathcal{L}_{H_2O} = 'wv'$

$c_p^{(\ell)} = c_p^{(d)}$

(94) ←

(ice reference enthalpy, $\bar{\tilde{T}}_s \equiv \bar{T}_{atm,s} = \bar{T}_{surf,s}$)

Now also assume that the energy equation is valid for grid mean values in the model (**QUESTIONABLE ASSUMPTION!**)



“Enthalpy flux” plan

Assume:

- Primitive equations (hydro)
- Assume model top pressure
- All components of moist a
- Assume that water enterin
- leaving the atmosphere (o

Switch to variable latent heats (to be consistent w/ MOM6)
 (note: **FV3 and SE already use variable latent heats**)

Lauritzen et al. (2022, in prep)

- change CAM’s thermodynamic variable (%s) to use variable latent heats
- if parameterizations use constant latent heat assumption that needs to be changed

ental velocity
 e temperature as water
ACCURATE!

Then it can be shown that the following globally integrated total energy eq.

Many models make these assumptions:

$$\frac{\partial}{\partial t} \iiint \rho^{(d)} \left\{ \bar{K} + \bar{\Phi}_s + c_p^{(d)} \bar{T} + \sum_{\ell \in \mathcal{L}_{H_2O}} m^{(\ell)} \left[\bar{K} + \bar{\Phi}_s + c_p^{(\ell)} (\bar{T} - T_{00}) + h_{00}^{(ice)} \right] + \bar{m}^{(wv)} L_{s,00} + \bar{m}^{(liq)} L_{f,00} \right\} dA dz$$

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$c_p^{(\ell)} = c_p^{(d)}$

(94) ←

(ice reference enthalpy, $\bar{\tilde{T}}_s \equiv \bar{T}_{atm,s} = \bar{T}_{surf,s}$)

Now also assume that the energy equation is valid for grid mean values in the model (**QUESTIONABLE ASSUMPTION!**)

“Enthalpy flux” plan

Explicit enthalpy flux term:

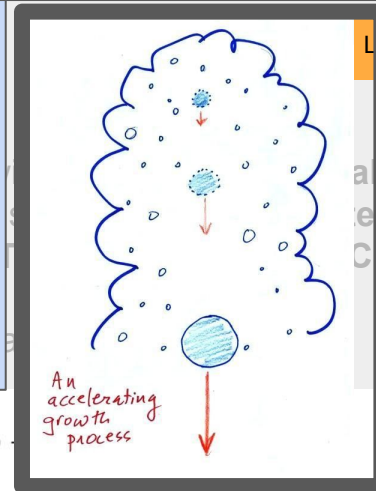
What temperature to use?

Evaporation : surface T (SST over ocean)

Precipitation : T where it was created? Neglects frictional heating

(note: “naturally” incorporated using barycentric velocity framework (Lauritzen et al., 2022))

T in lowest model level?



Lauritzen et al. (2022, in prep)

velocity
temperature as water
ACCURATE!

Many models make these assumptions:

$$\frac{\partial}{\partial t} \iiint \rho^{(d)} \left\{ \bar{K} + \bar{\Phi}_s + c_p^{(d)} \bar{T} + \bar{\Phi}_s + c_p^{(\ell)} (\bar{T} - T_{00}) + \bar{m}^{(wv)} L_{s,00} + \bar{m}^{(liq)} L_{f,00} \right\} dA dz$$

$$= \iint \left\{ \sum_{\ell \in \mathcal{L}_{H_2O}} F_{net}^{(\ell)} \left[\bar{K}_s + \bar{\Phi}_s + c_p^{(\ell)} (\bar{T}_s - T_{00}) + h_{00}^{(ice)} \right] + \bar{F}_{net}^{(wv)} L_{s,00} + \bar{F}_{net}^{(liq)} L_{f,00} + \bar{F}_{net}^{(turb,rad)} \right\} dA.$$

(94) ←

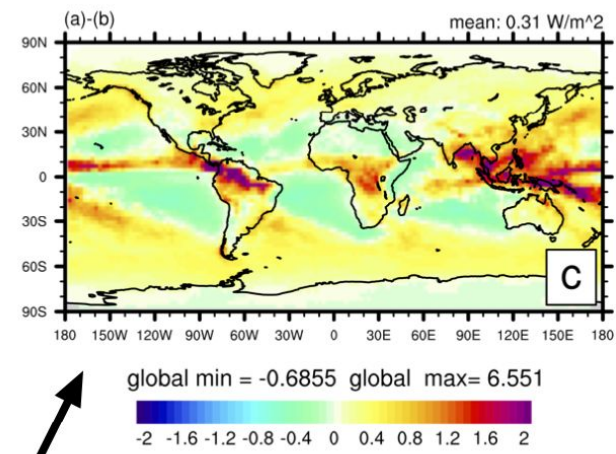
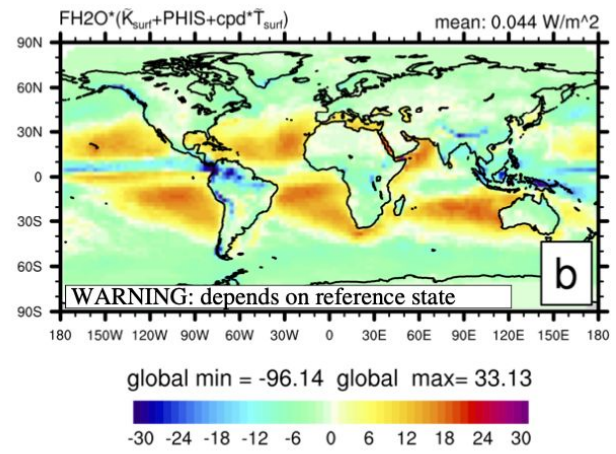
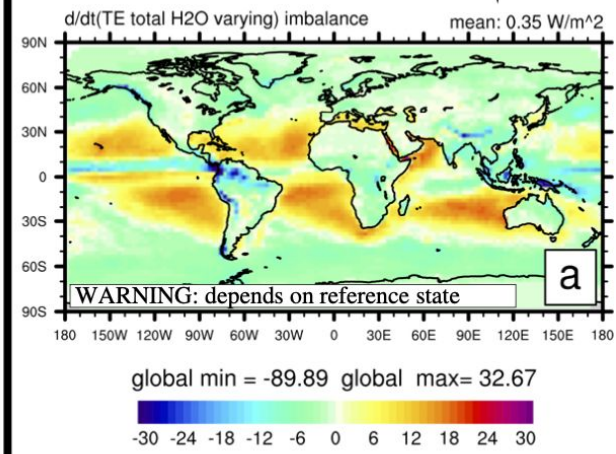
(ice reference enthalpy, $\bar{T}_s \equiv \bar{T}_{atm,s} = \bar{T}_{surf,s}$)

Now also assume that the energy equation is valid for grid mean values in the model (QUESTIONABLE ASSUMPTION!)

Modified CAM total energy equation incl. missing flux terms

$$\frac{\partial}{\partial t} \int \bar{\rho}^{(d)} \left\{ \left(1 + \bar{m}^{(H_2O)} \right) \left[\bar{K} + \bar{\Phi}_s + c_p^{(d)} (\bar{T} - T_{00}) \right] + \bar{m}^{(wv)} L_{s,00} + \bar{m}^{(liq)} L_{f,00} \right\} dz$$

$$- \Delta \hat{\mathcal{I}}_{\partial m^{(H_2O)}/\partial t} - \Delta \mathcal{I}_{m_{t_n}^{(H_2O)}} = \bar{F}_{net}^{(H_2O)} \left[c_p^{(d)} (\tilde{T}_s - T_{00}) + \tilde{K}_s + \bar{\Phi}_s \right] + \bar{F}_{net}^{(wv)} L_{s,00} + \bar{F}_{net}^{(liq)} L_{f,00} + \bar{F}_{net}^{(turb,rad)}$$







Why does CESM have multiple atmosphere dynamical cores?



- To assess (structural) uncertainty due to dynamical core one needs more than 1 dynamical core
- Dynamical cores are strongly depending on compute platform and programming paradigm (MPI communication, vectorization,...); supercomputing environment is constantly changing!
- Dynamical core science is not settled though many strong opinions in the community
- CESM is unique in that it enables “advanced” dynamical core science in the sense of having idealized to full climate functionality with multiple dynamical cores in one system!

Slide from P. Neilley

(Director of Weather Forecasting Sciences, Technologies and Operations at IBM's Weather Company)

First Symposium on Earth Prediction Innovation and Community Modeling
at AMS, 2022

Looking Ahead: A Few Cautions

1. How many modelling communities is too many?
 - Critical mass is essential to get $1+1=3$
 - Can we avoid dynamic core/ component organized communities?
 - Is a community super-model with multiple dynamic cores possible?
2. Narrow motives -> disappointing outcomes
 - Avoid "My model for my use" motive
 - Catalyze, encourage and celebrate broad creative uses to benefit the science and society.
 - Breadth of adoption should be a core metric of success





Total energy

Imbalance of incl. all forms of water in CAM's parameterization total energy equation:



Assume:

- Primitive equations (hydrostatic, shallow)
- Assume model top pressure is constant
- All components of moist air have the same
- Assume that water entering the atmosphere is leaving the atmosphere (dew, liquid and

Then it can be shown that the following global

Many models make these assumptions:

$$\frac{\partial}{\partial t} \iiint \rho^{(d)} \left\{ \bar{K} + \bar{\Phi}_s + c_p^{(d)} \bar{T} + \overline{wv'} \right. + \left. \overline{m} \right\}$$

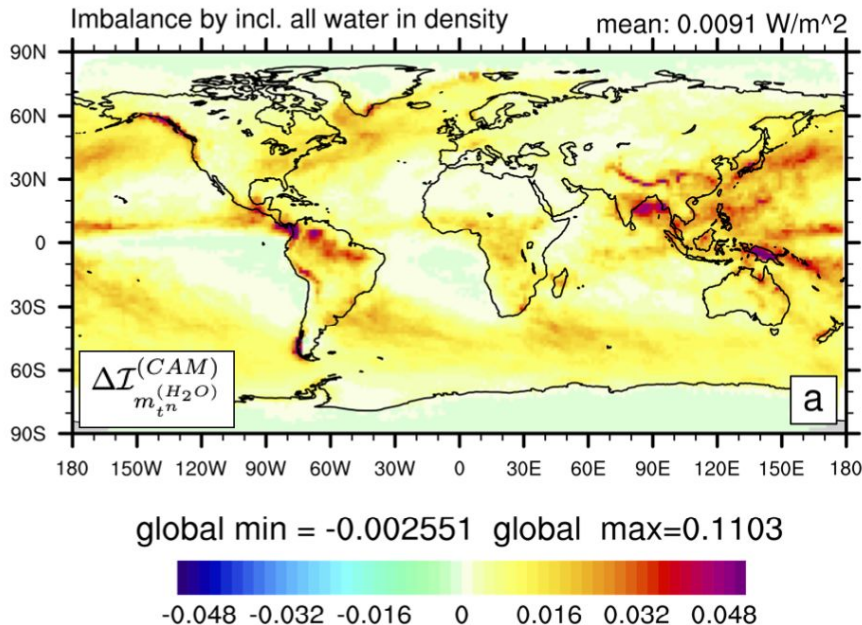
$$= \iint \left\{ \sum_{\ell \in \mathcal{L}_{cond}} F_{net}^{(\ell)} \left[\bar{\tilde{K}}_s + \bar{\Phi}_s + c_p^{(d)} \bar{T} \right] \right.$$

(ice reference)

Now also assume that the energy equation is **ASSUMPTION!**

$$\Delta \mathcal{I}_{m_{tn}^{(H_2O)}}^{(CAM)} =$$

$$\int \left[\rho^{(d)} \left(\sum_{\ell \in \mathcal{L}_{cond}} \bar{m}_{tn}^{(\ell)} \right) \right] \frac{\partial}{\partial t} \left(\bar{K} + \bar{\Phi}_s + c_p^{(d)} \bar{T} \right) dz$$



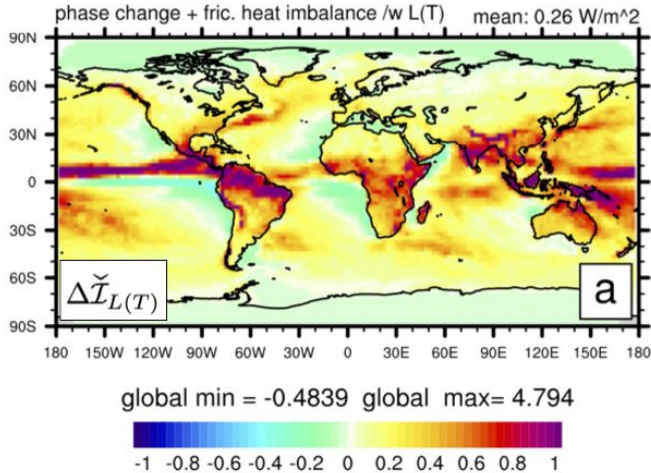
velocity
temperature as water
RATE!

E

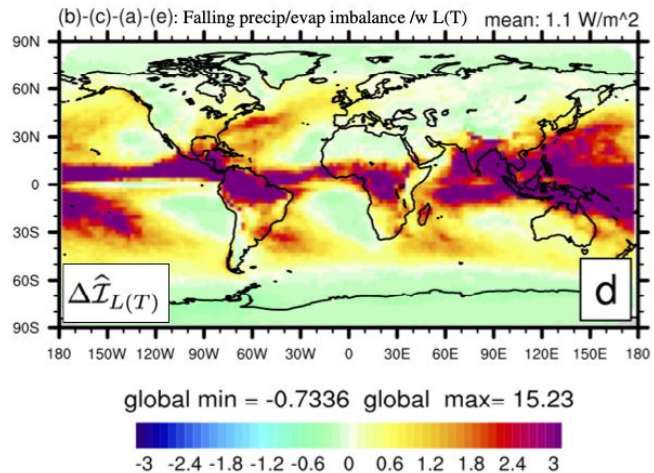
Modified (consistent) total energy equation assuming variable latent heats

$$\frac{\partial}{\partial t} \int \bar{\rho}^{(d)} \left\{ \underbrace{\left(1 + \bar{m}^{(H_2O)}\right) \left(\bar{K} + \bar{\Phi}_s\right) + c_p^{(d)} T + \sum_{\ell \in \mathcal{L}_{H_2O}} \bar{m}^{(\ell)} c_p^{(\ell)} \left(\bar{T} - T_{00}\right) + \bar{m}^{(wv)} L_{s,00} + \bar{m}^{(liq)} L_{f,00}}_{\text{...}} \right\} dz$$

$$-\Delta \tilde{\mathcal{I}}_{L(T)} - \Delta \hat{\mathcal{I}}_{L(T)} = - \sum_{\ell \in \mathcal{L}_{H_2O}} \bar{F}_{net}^{(\ell)} \left[c_p^{(\ell)} \left(\tilde{T}_s - T_{00}\right) + \tilde{K}_s \right] + \bar{F}_{net}^{(wv)} L_{s,00} + \bar{F}_{net}^{(liq)} L_{f,00} + \bar{F}_{net}^{(turb,rad)}$$



(a) Imbalance for processes not involving falling precip. & evap.



(b) Imbalance for falling precip. & evap.